



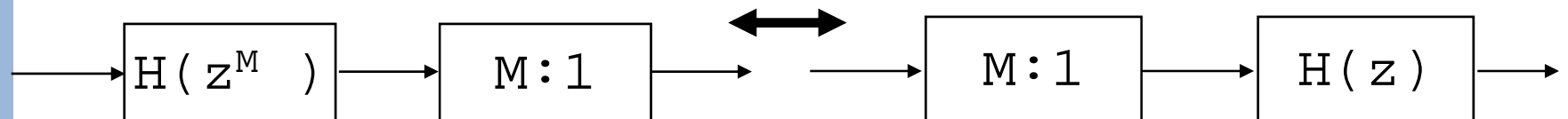
Multirate Filtering, Resampling Filters, Polyphase Filters

or how to make efficient FIR
filters



THE NOBLE IDENTITY 1

Efficient Implementation of Resampling filters

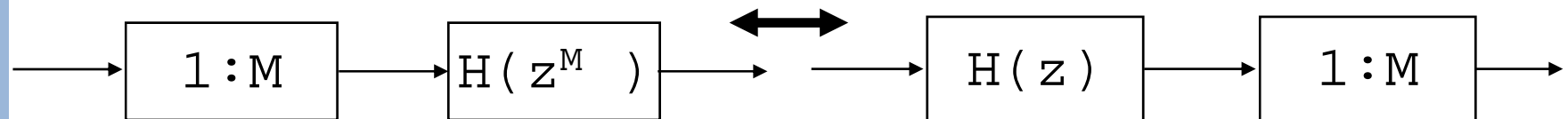


Rule 1: Filtering with M -unit delays followed by a $M:1$ downsampling is equivalent to $M:1$ downsampling followed by filtering with 1 unit delays.



THE NOBLE IDENTITY 2

Efficient Implementation of Resampling filters



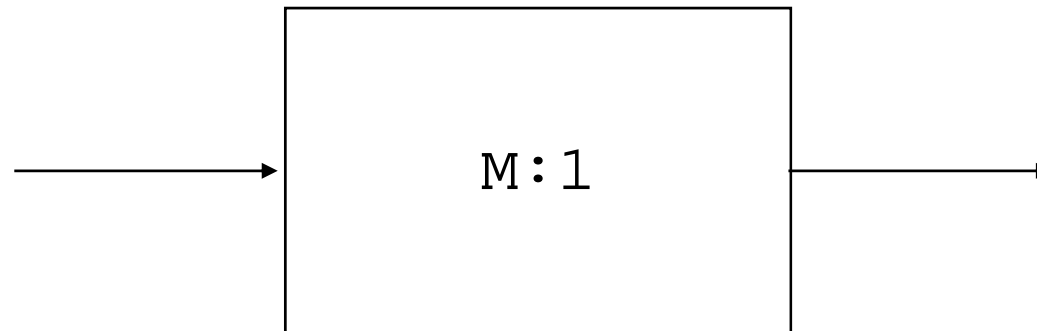
Rule 2: $1:M$ upsampling followed by filtering with M -unit delays is equivalent to filtering with 1 unit delays followed by $1:M$ upsampling.

It is always more efficient to apply the filter at the lower sample rate



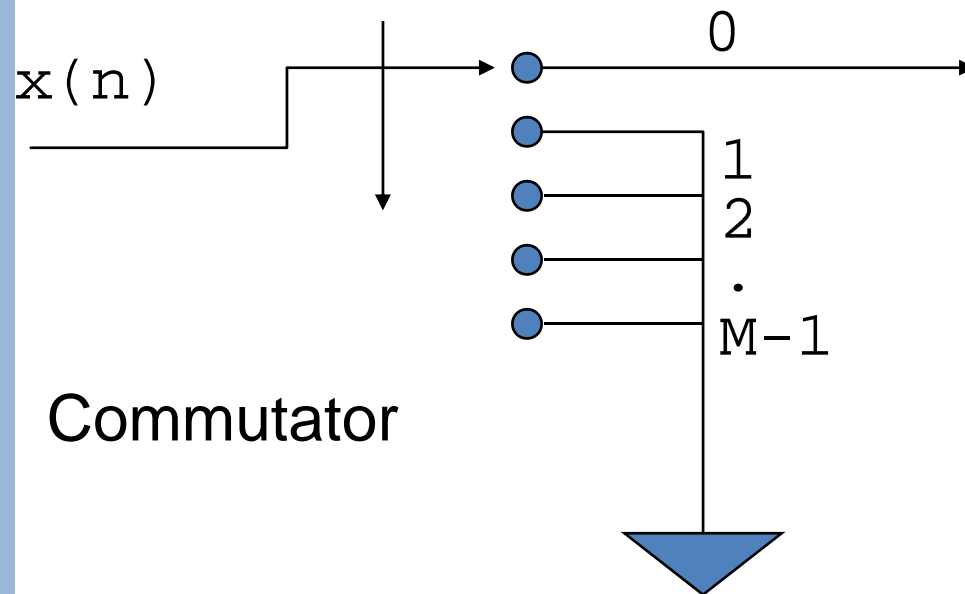
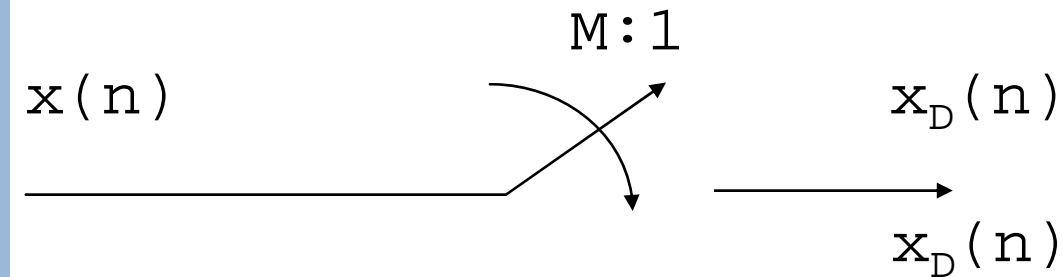
Downsampling

- Sometimes called *decimation*. This is poor nomenclature since decimation refers to removing 1 in 10.
- It is useful to think of the downsampling operation as the output of a commutator.





Downsampling

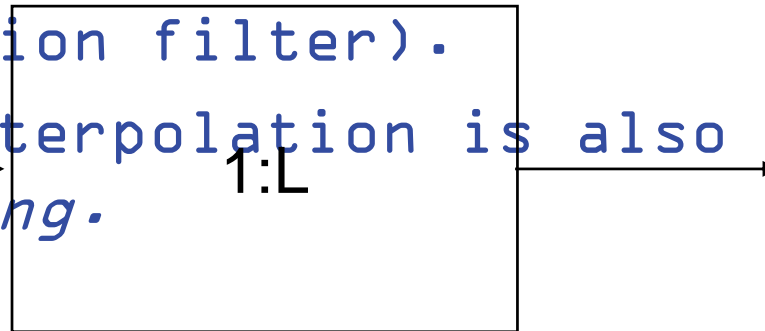


If $x(n)$ has samples indexed from 0 to $N-1$, then $x_D(n)$ has samples indexed from 0 to $(N/M)-1$.



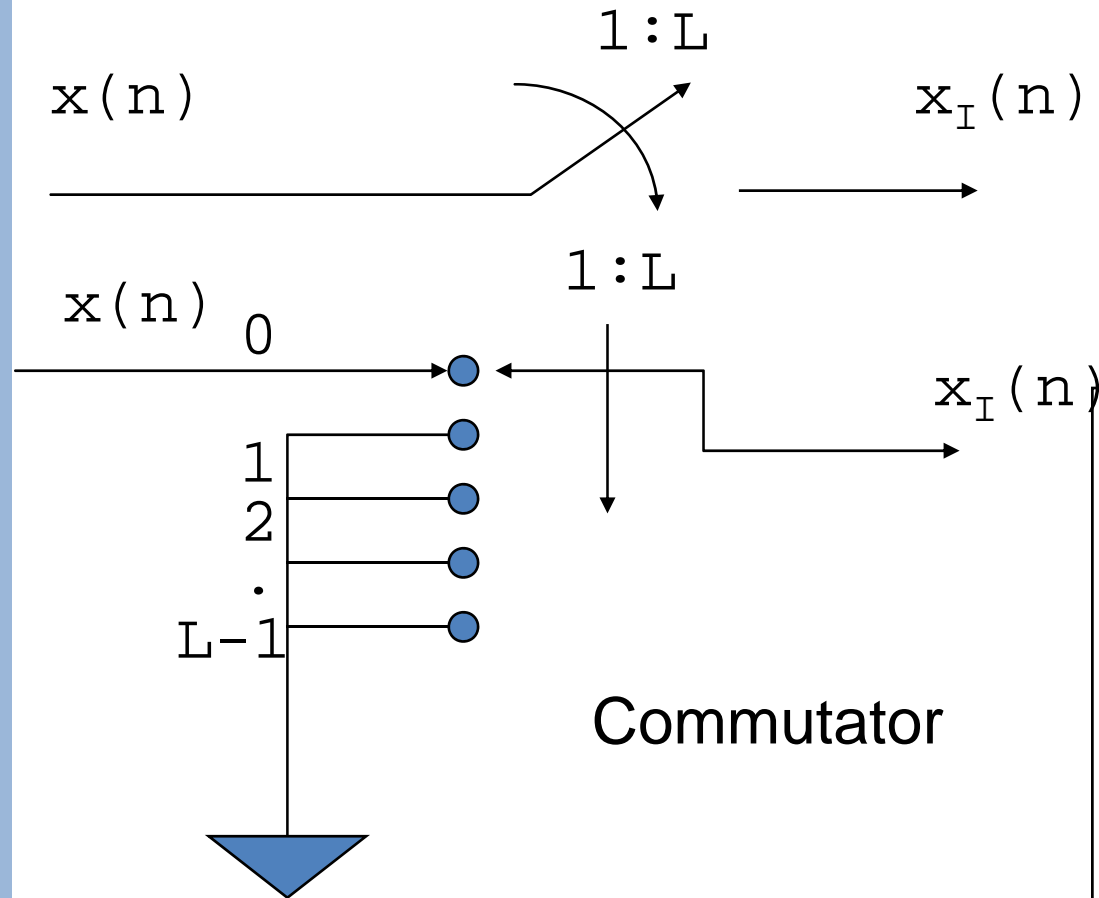
Upsampling

- Sometimes called *interpolation* although it is not interpolation in the conventional sense; it is just putting zeros between samples. If we wish to perform interpolation in the conventional sense, we must pass the DSP interpolated data through a low pass filter (anti-imaging or interpolation filter).
- In DSP, interpolation is also called *zero-padding*.





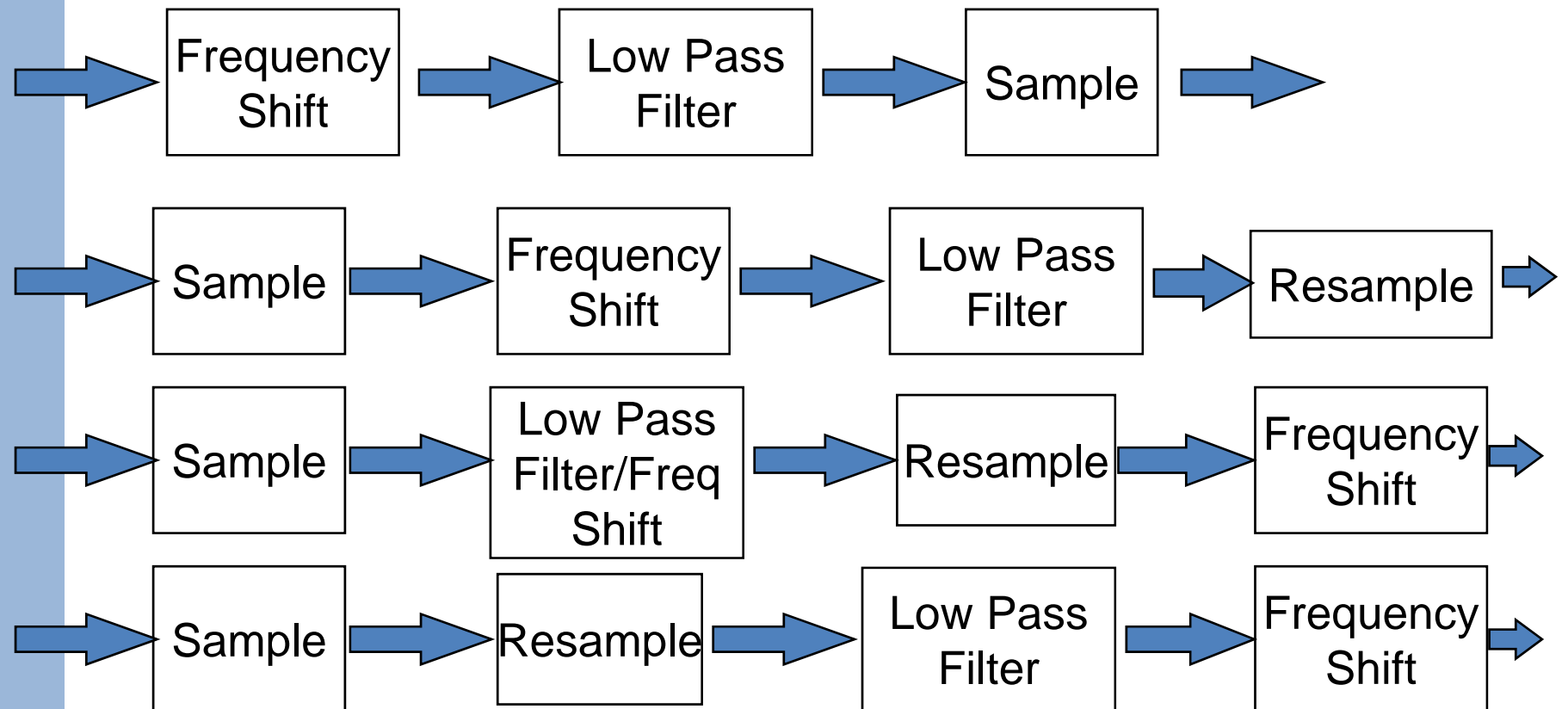
Upsampling

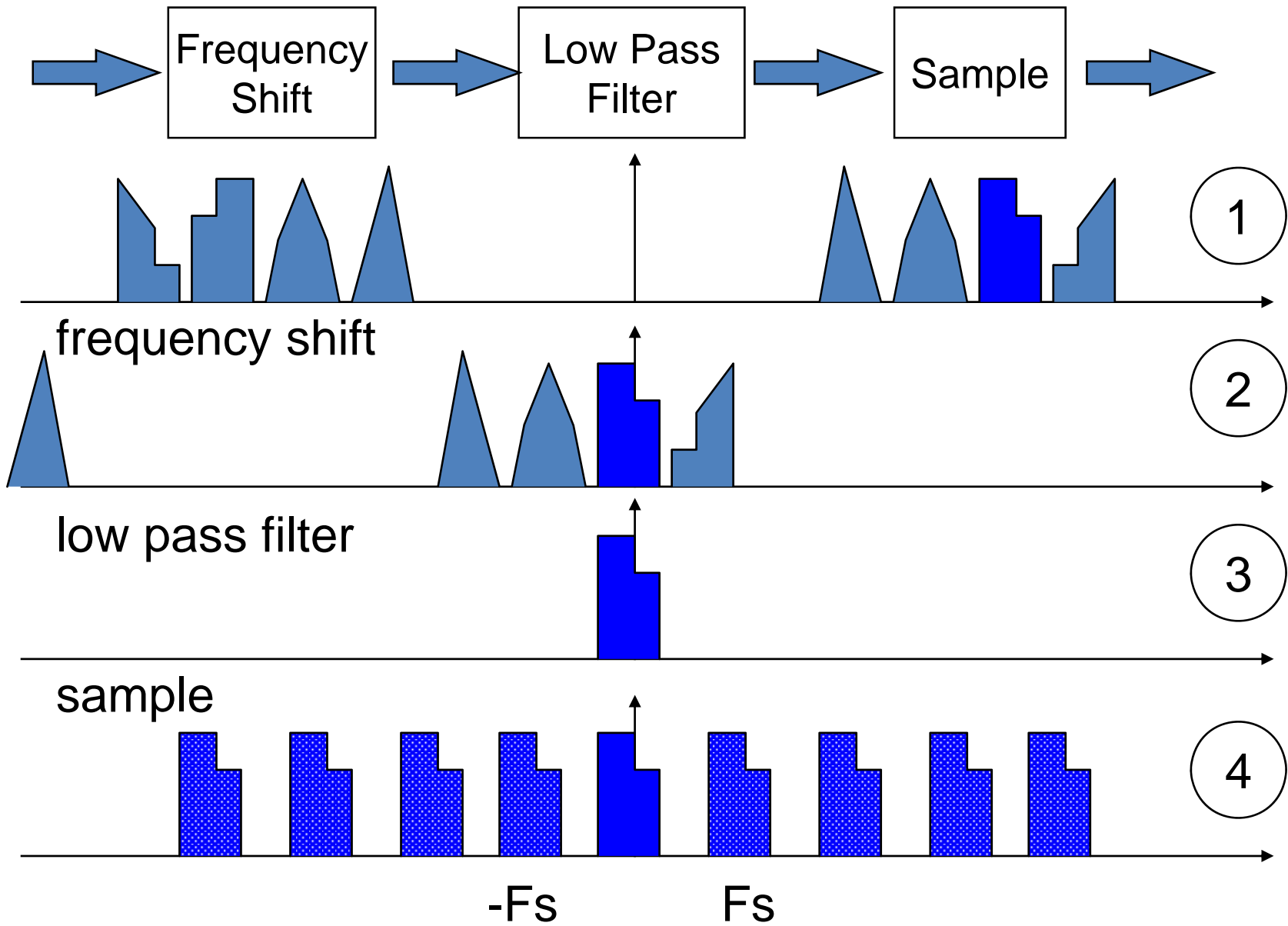


If $x(n)$ has samples indexed from 0 to $N-1$, then $x_I(n)$ has samples indexed from 0 to $LN-1$.



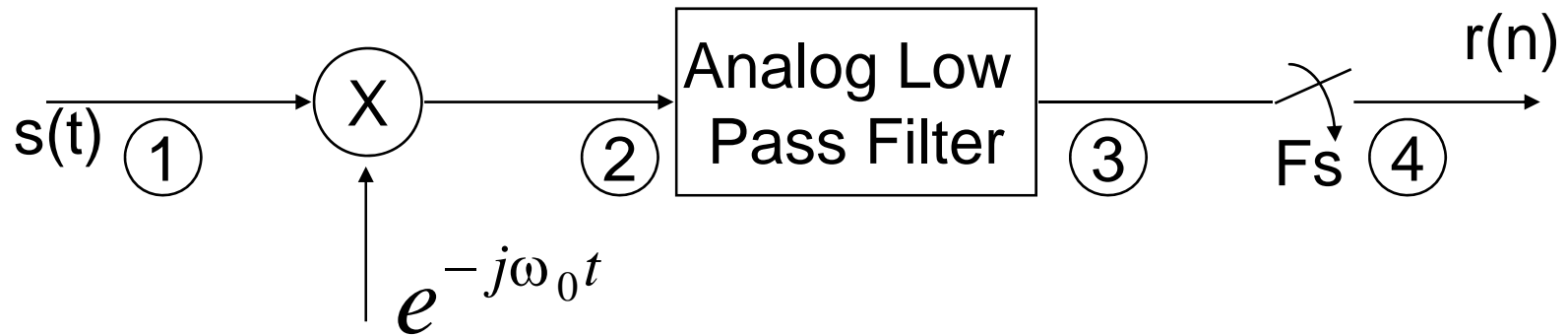
Digital Receiver Options



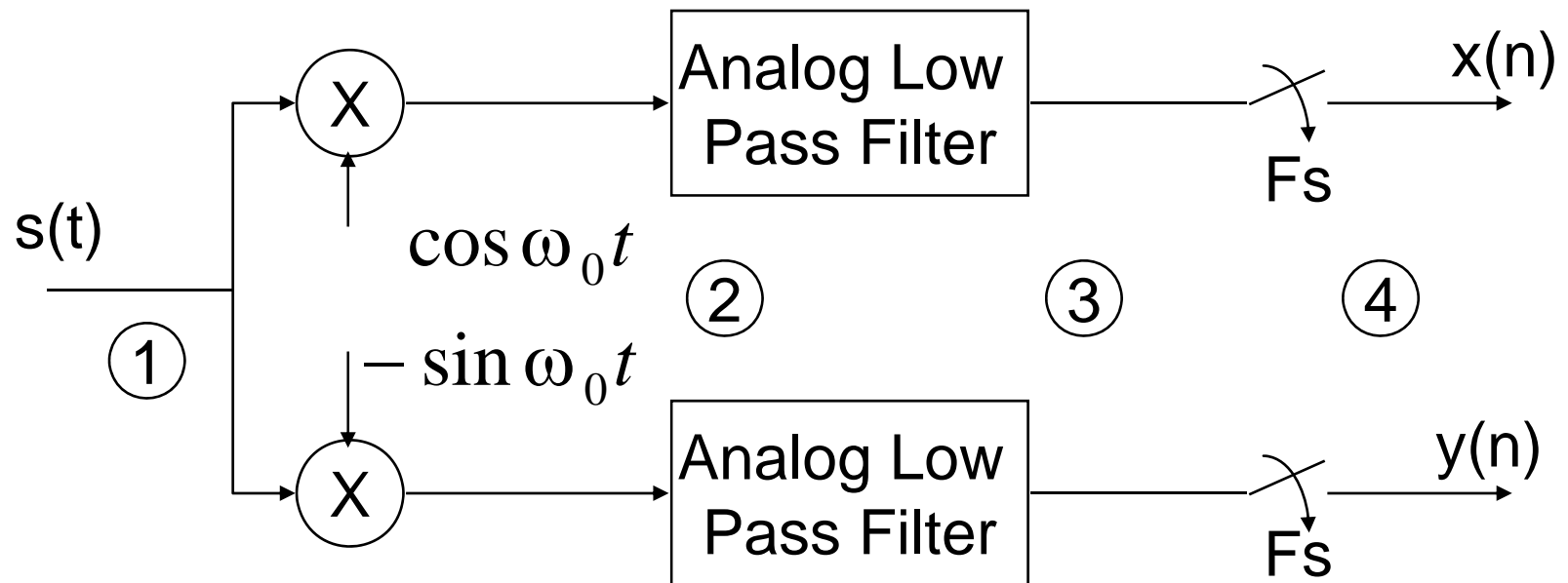




Receiver Structure



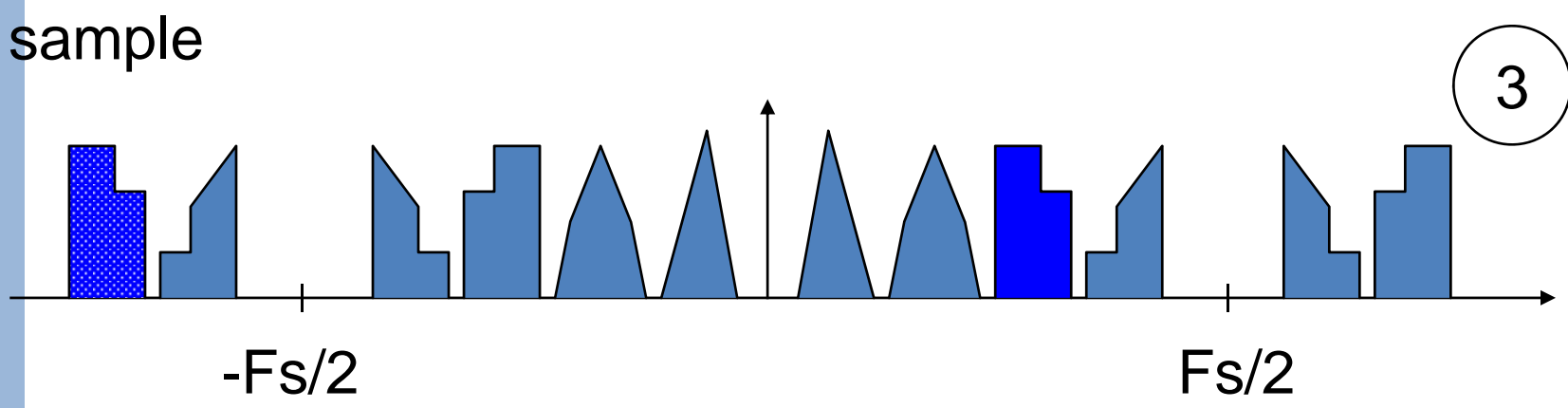
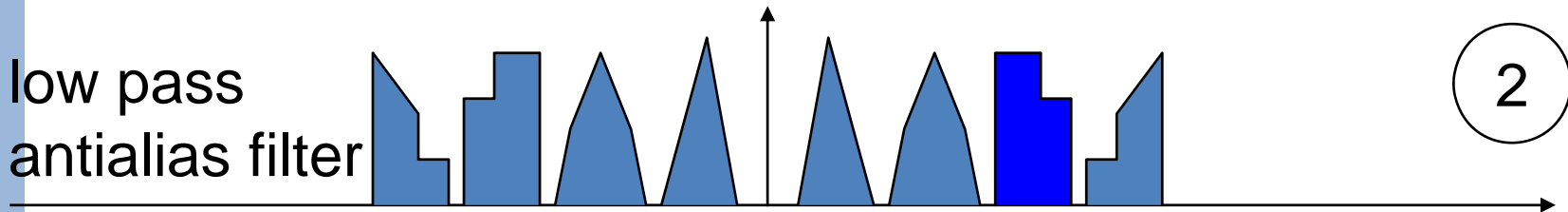
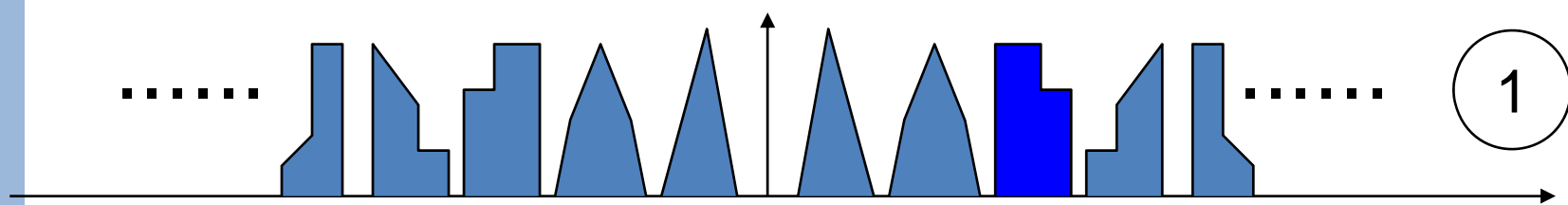
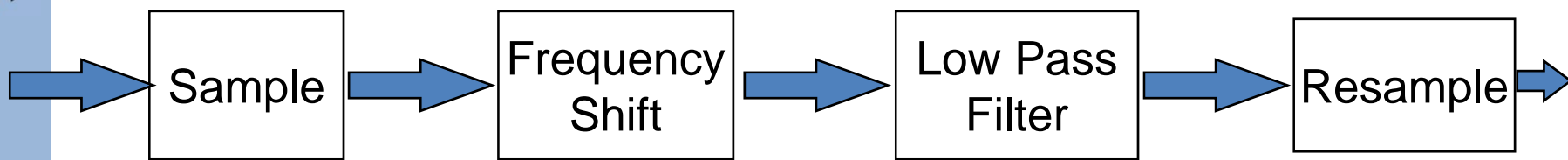
Which can be implemented by





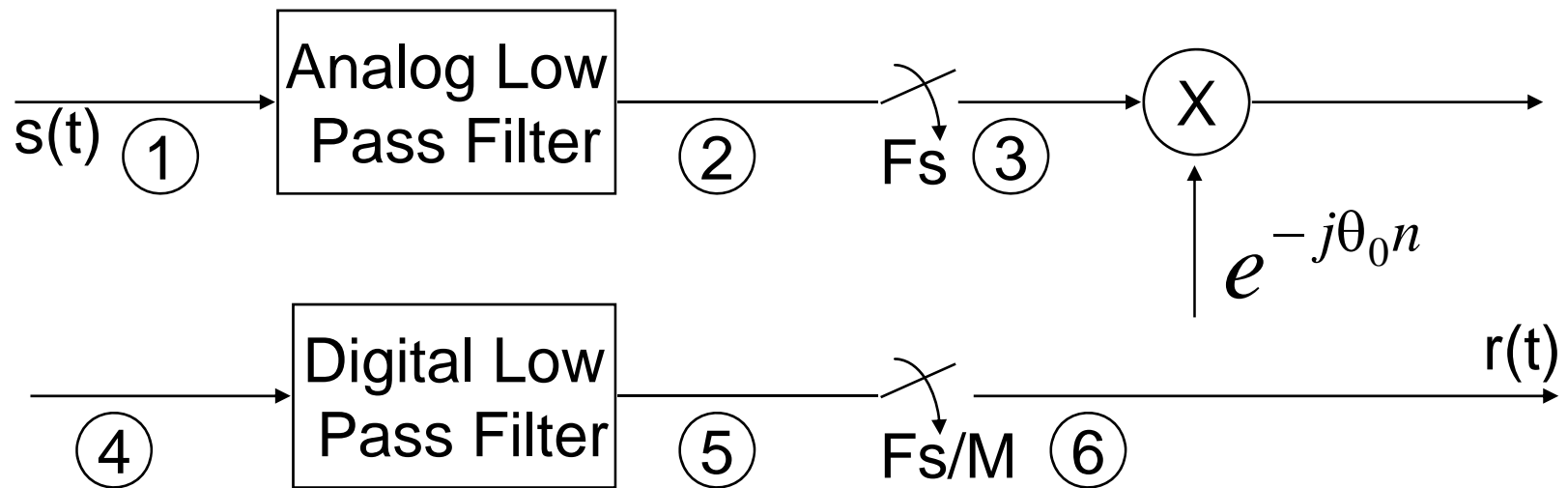
Comments

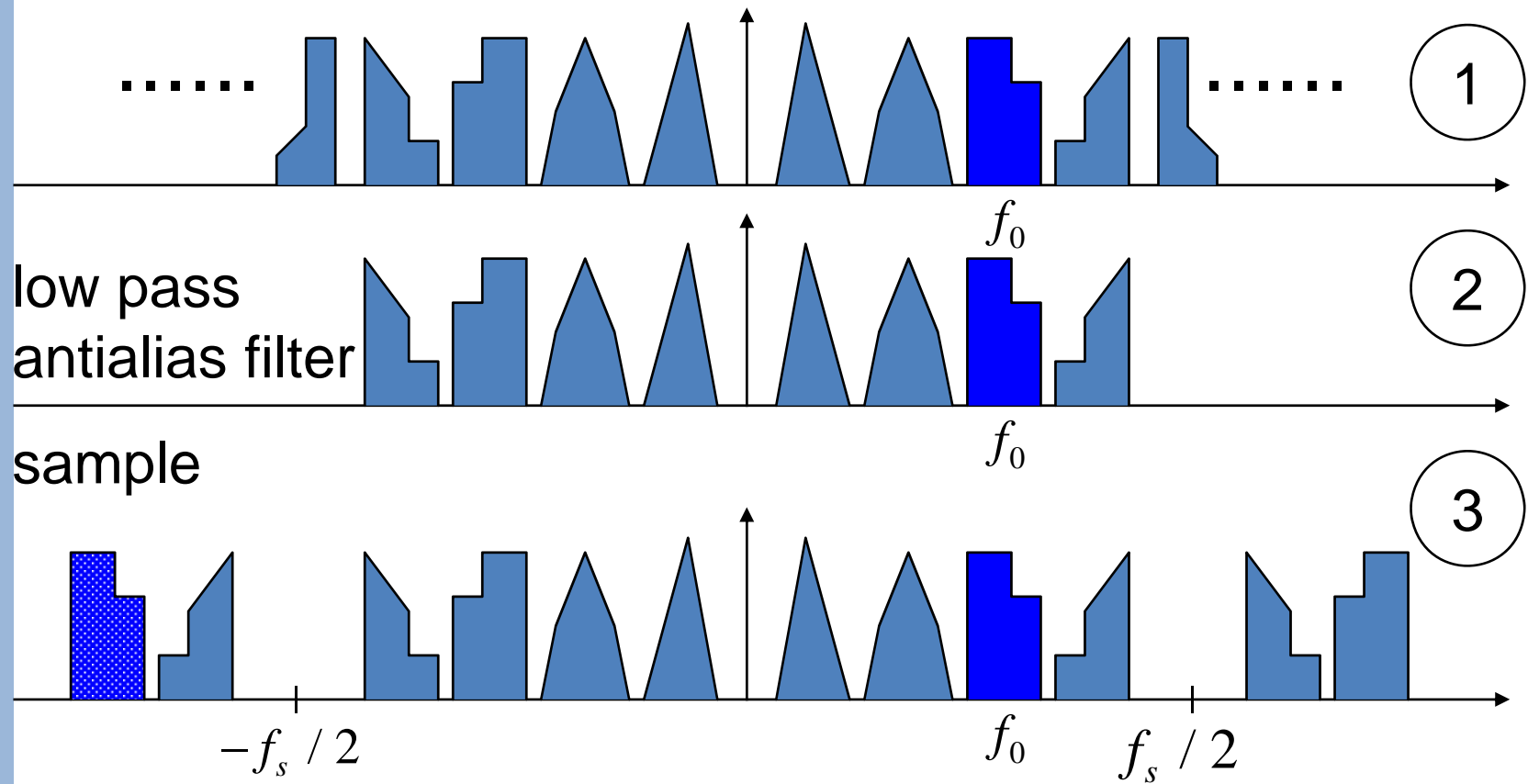
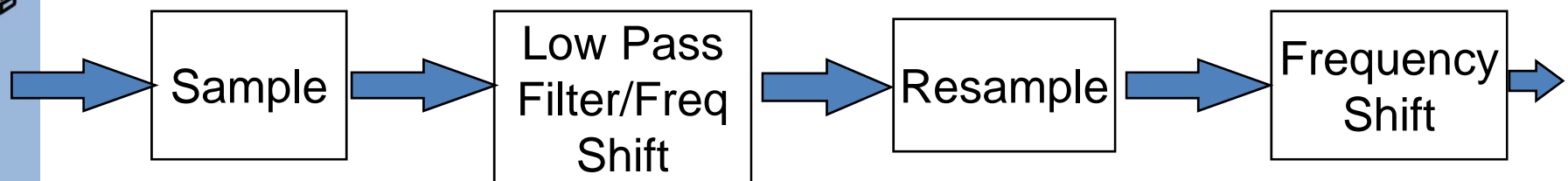
- Need to have
 - two perfectly matched analog mixers
 - two perfectly matched high order analog filters
 - two perfectly matched analog-to-digital converters
- Difficult to achieve and expensive
- Reduce expense by performing some of these operations in DSP





Receiver Structure

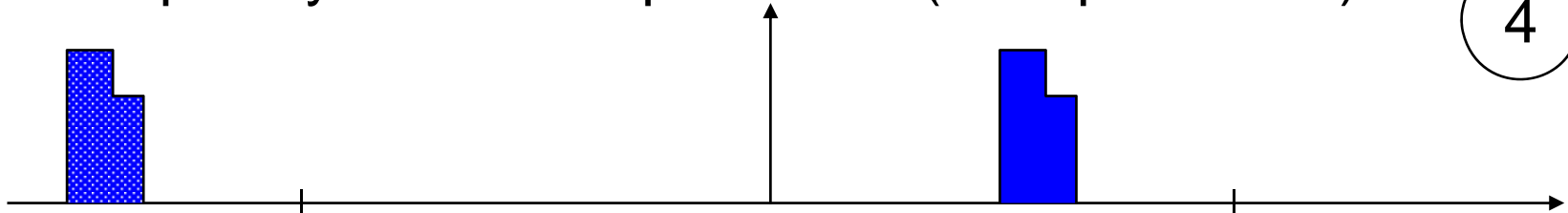






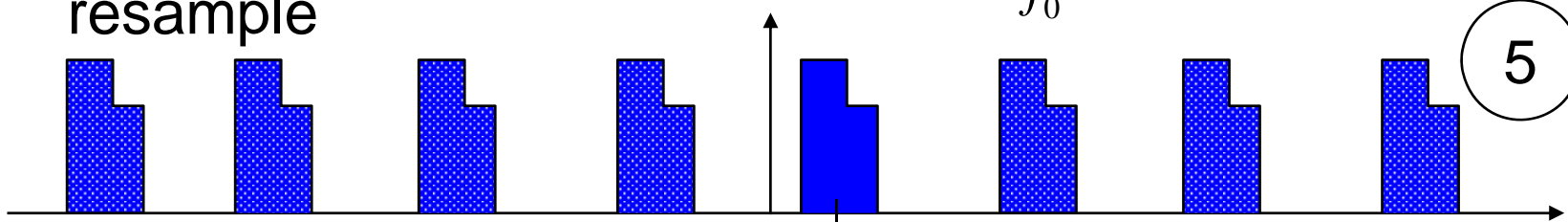
frequency shifted lowpass filter (bandpass filter)

4



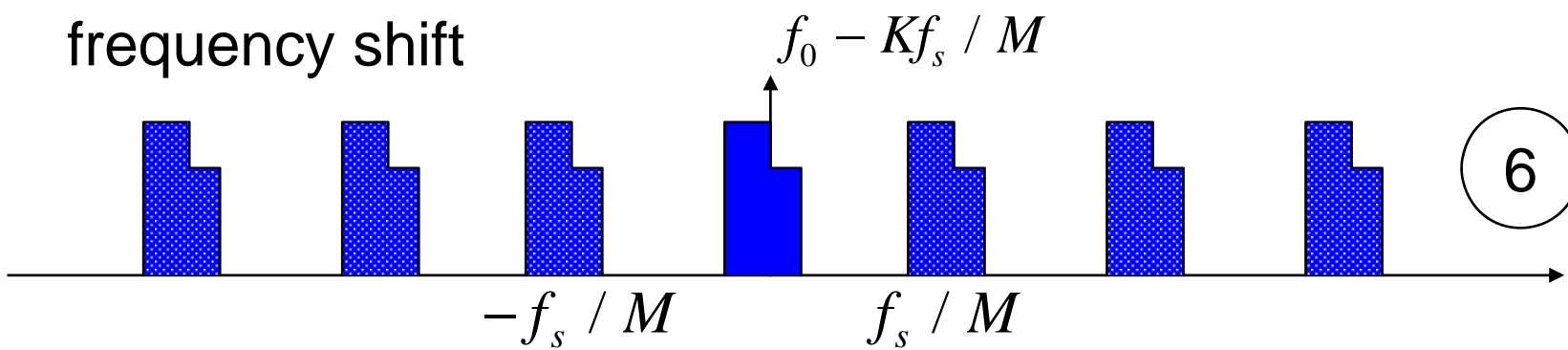
resample

5



frequency shift

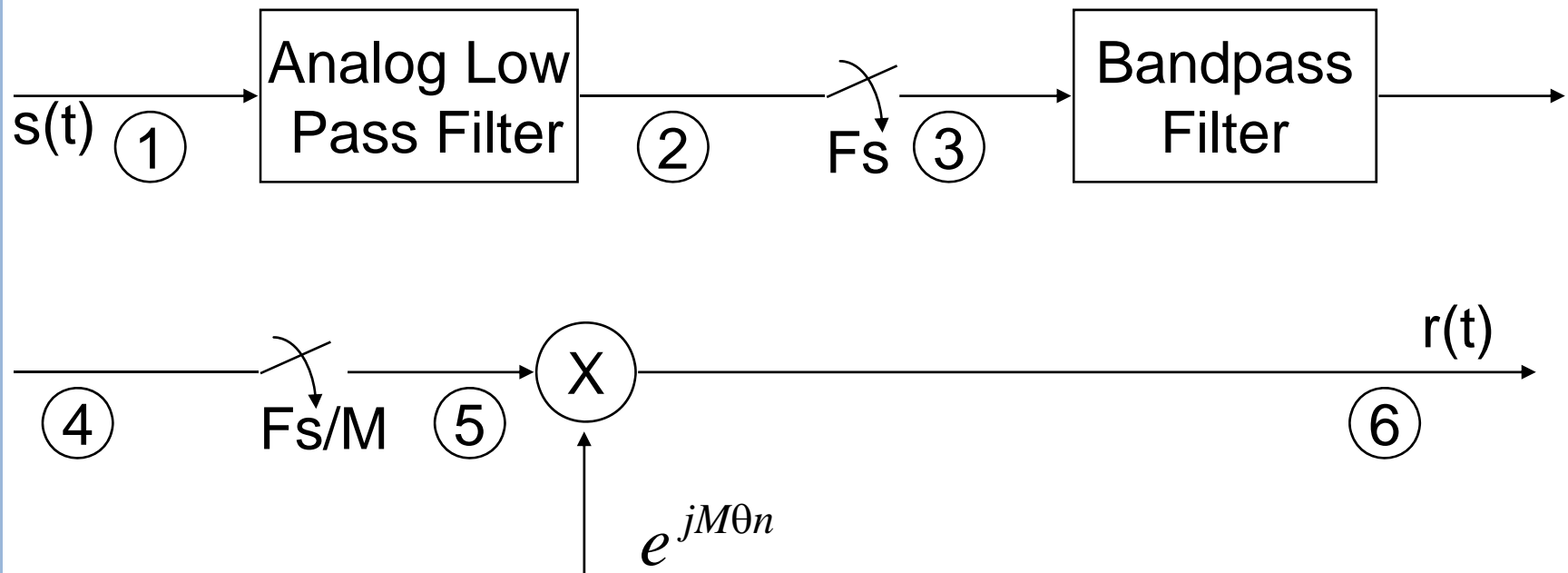
6



$f_s / M > \text{two sided bandwidth}$



Receiver Structure



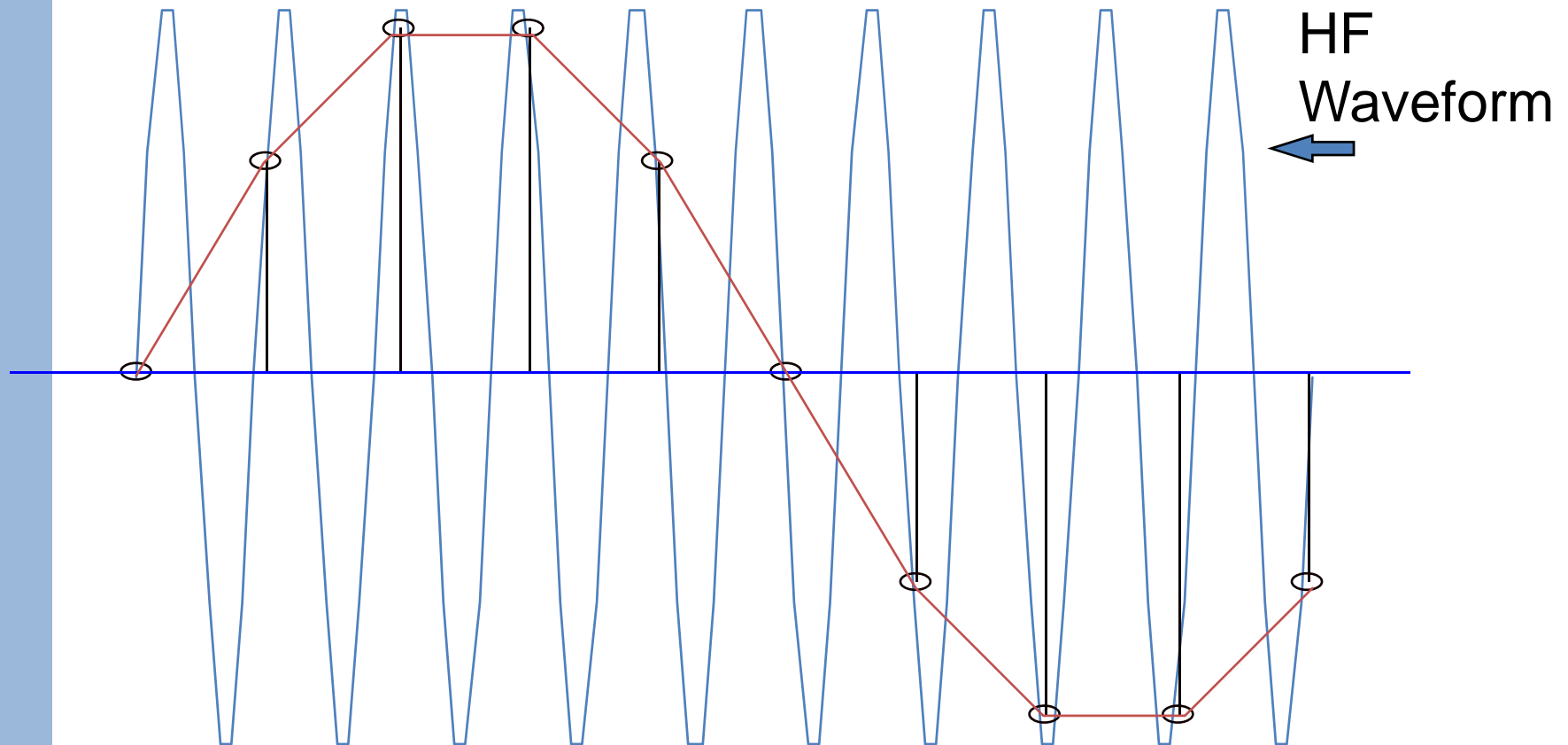


Comments

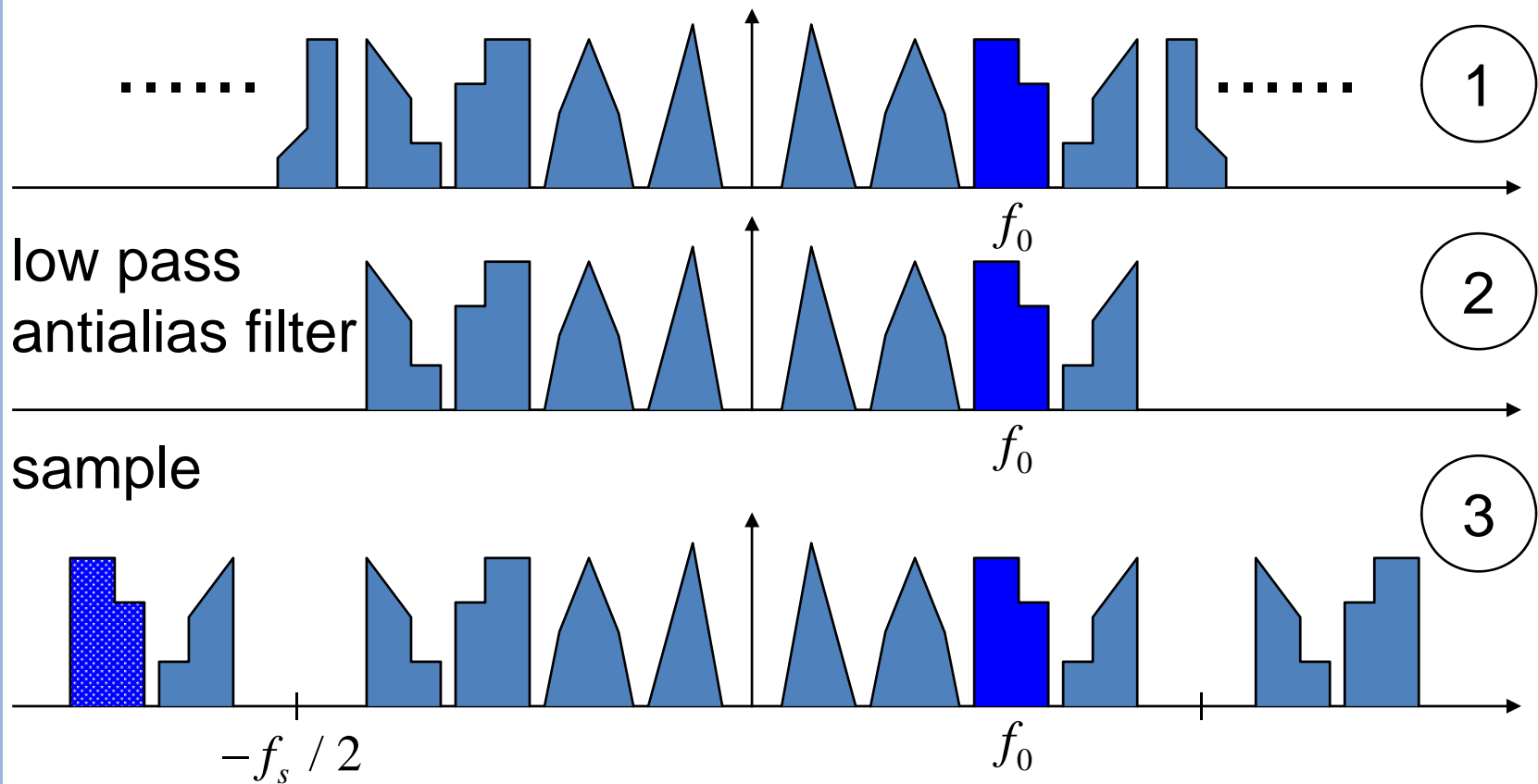
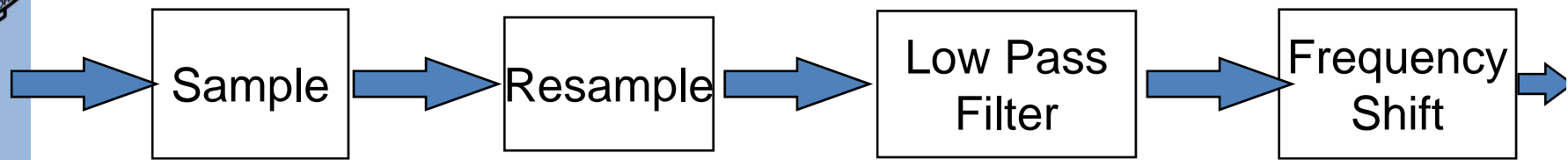
- No need to frequency shift signal to baseband before resampling.
- As long as the sampling frequency is greater than the two sided bandwidth, no information will be lost due to aliasing.
- This condition is sufficient even if the signal is passband although the resampling may appear to cause a frequency shift.
- This technique is exploited in sampling oscilloscopes which capture very high frequency signals with low sampling rates.



Sampling Oscilloscope Principle

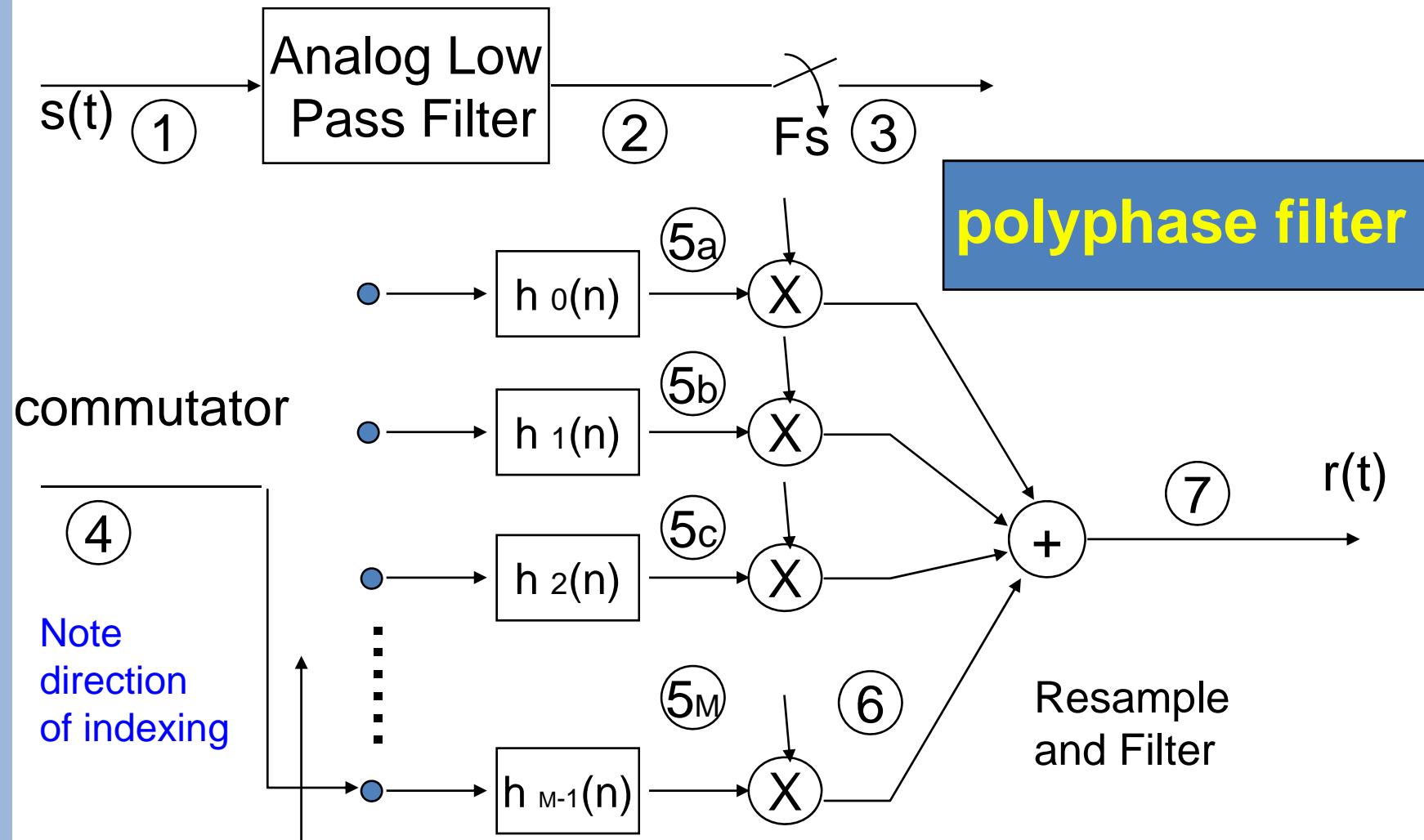


Sampled data is a time scaled version of HF waveform





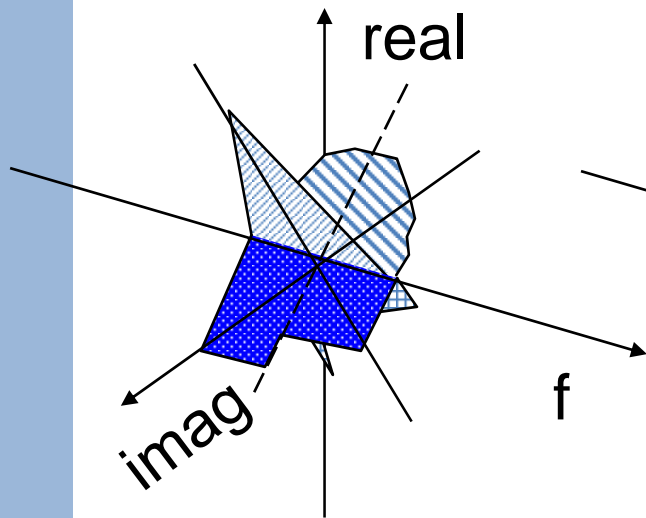
Receiver Structure



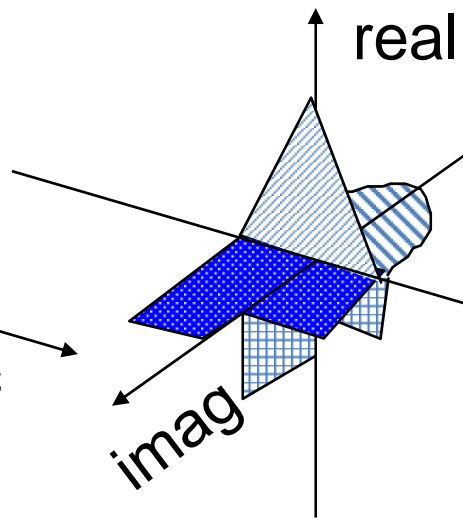


resample

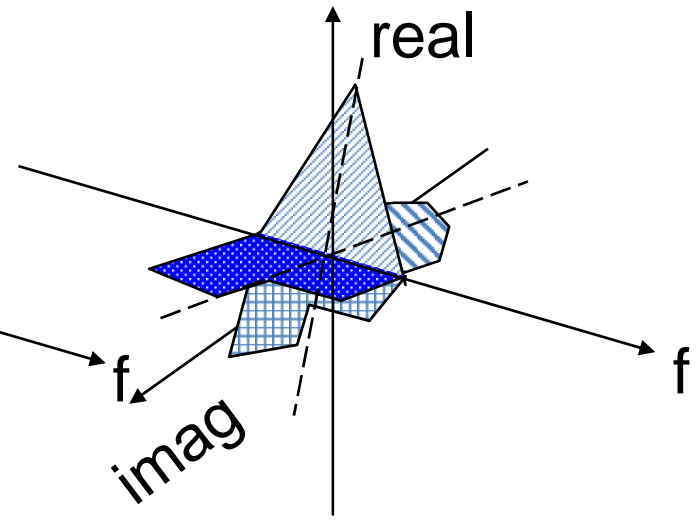
5a



5b



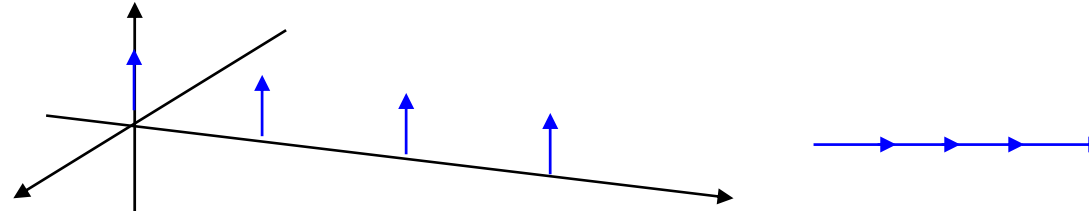
5c



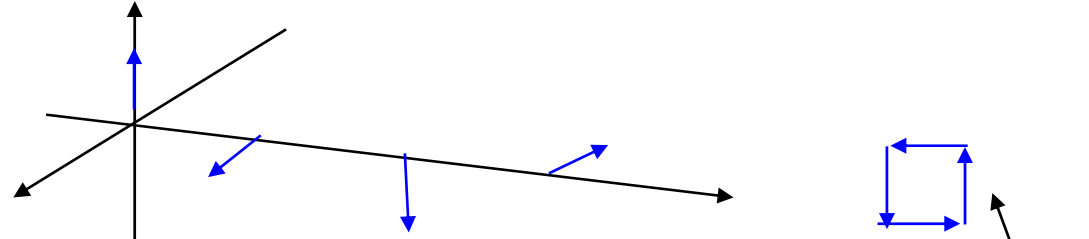


Delay

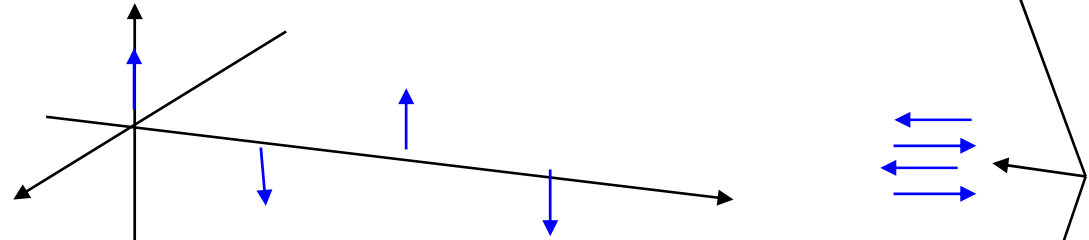
$t=0.T/4$



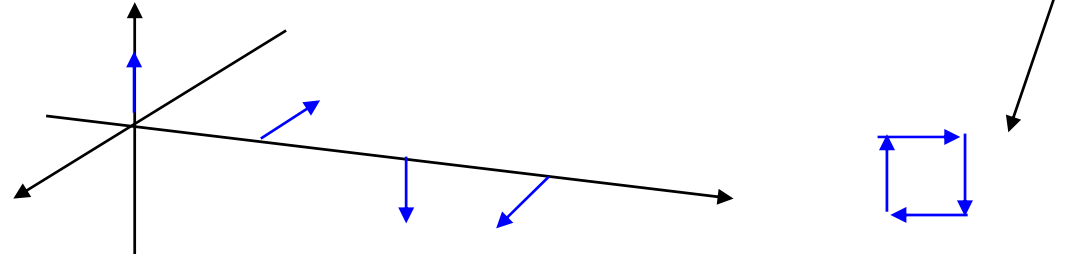
$t=1.T/4$



$t=2.T/4$



$t=3.T/4$



cancel



Comments

- In the polyphase filter design we introduce deliberate aliasing by downsampling. Thus at the output of each filter, the desired signal is jumbled up with replicas of the other unwanted bands.
- Due to the phase delays in the separate paths through the filter, the signals in the unwanted bands will cancel at the summing node leaving only the desired signal.
- This structure is computationally more efficient than the previous bandpass filter design (by a factor of M).



Polyphase Filter Partition

Let $N = L * M$

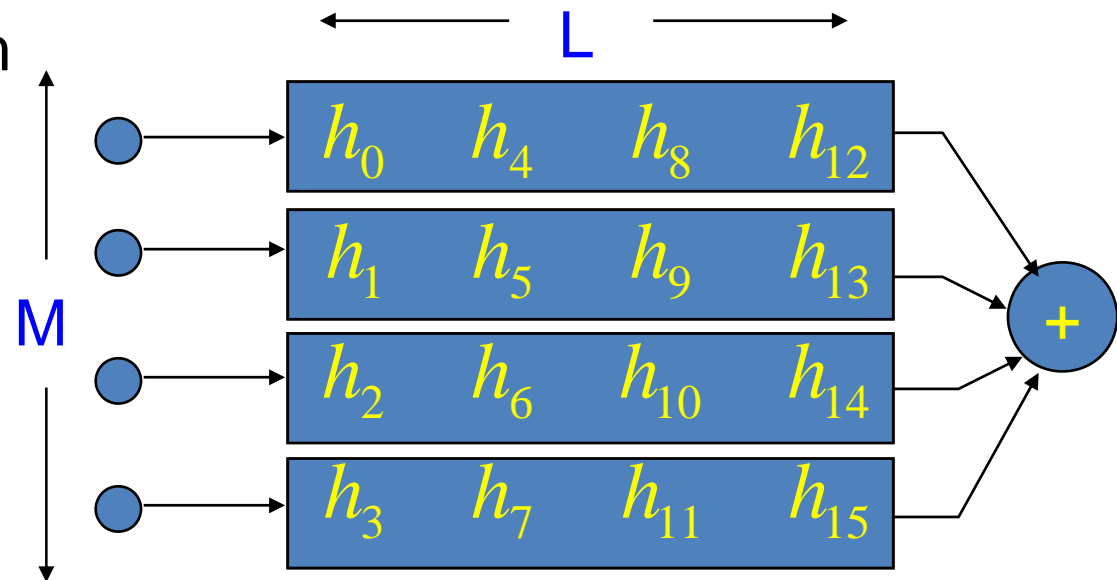
N = Filter Length

M = Resampling Rate

L = Subfilter Length

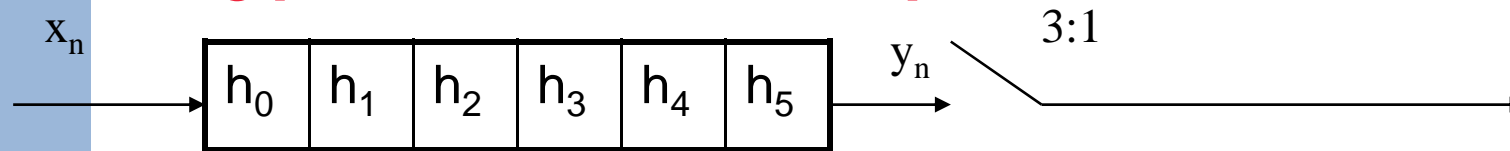
Note- can always zero pad to make $N = L * M$

Place filter coefficients columnwise into an M by L matrix. Subfilters are the rows of the matrix.





Polyphase Downsampler in Detail



0: $y_0 = h_0x_0$

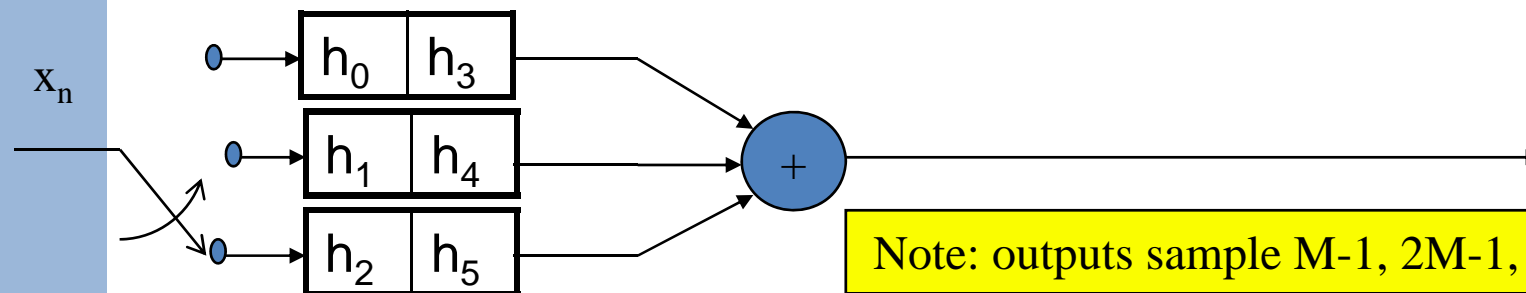
1: $y_1 = h_1x_0 + h_0x_1$

2: $y_2 = h_2x_0 + h_1x_1 + h_0x_2 \longrightarrow y_2 = h_2x_0 + h_1x_1 + h_0x_2$

3: $y_3 = h_3x_0 + h_2x_1 + h_1x_2 + h_0x_3$

4: $y_4 = h_4x_0 + h_3x_1 + h_2x_2 + h_1x_3 + h_0x_4$

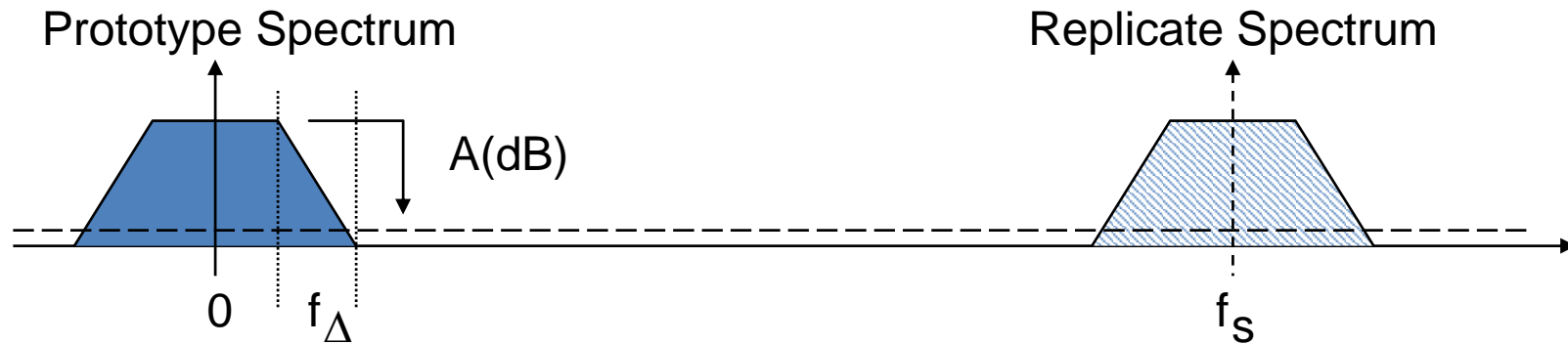
5: $y_5 = h_5x_0 + h_4x_1 + h_3x_2 + h_2x_3 + h_1x_4 + h_0x_5 \longrightarrow y_5 = h_5x_0 + h_4x_1 + h_3x_2 + h_2x_3 + h_1x_4 + h_0x_5$



Note: outputs sample $M-1, 2M-1, 3M-1 \dots$



Filter Design Equations



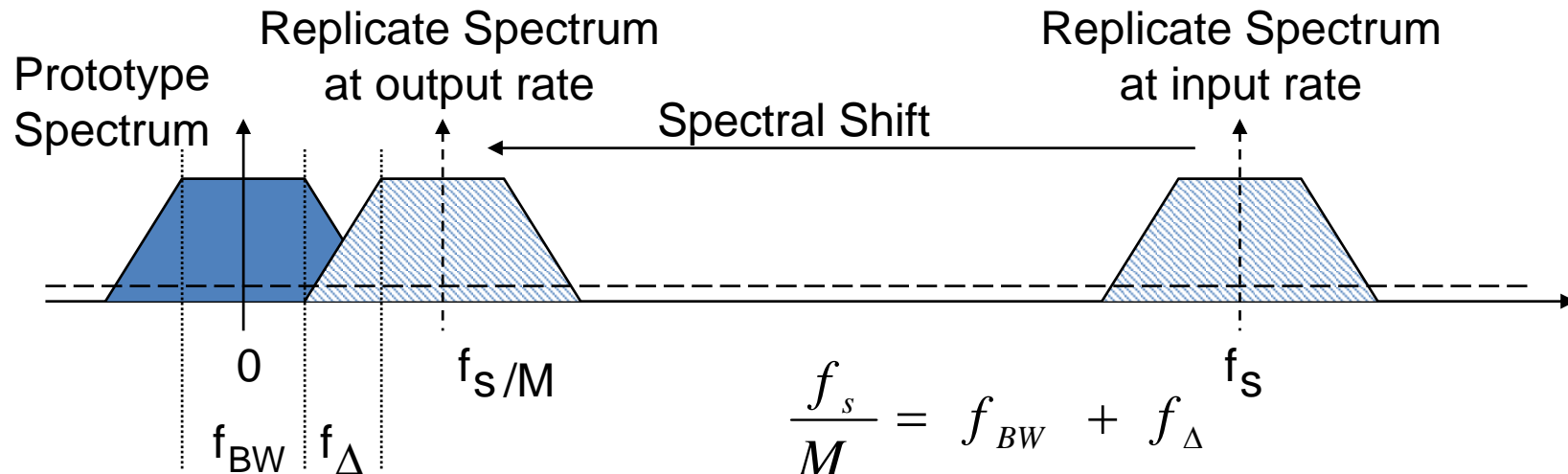
Example

$$f_{\Delta} = 200 \text{ Hz}$$

$$f_s = 20 \text{ kHz}$$

$$A(\text{dB}) = 80 \text{ dB}$$

$$\begin{aligned} N &= \frac{A(\text{dB})}{22} \frac{f_s}{f_{\Delta}} \\ &= \frac{80}{22} \frac{20,000}{200} \\ &= 364 \end{aligned}$$



$$f_{\Delta} = K(A) \frac{f_s}{N}; K(A) = \frac{A(\text{dB})}{22}$$

$$f_{BW} = a \frac{f_s}{M}$$

a = fractional bandwidth

$$\frac{f_s}{M} = \text{output sample rate}$$

$$\frac{f_s}{M} = f_{BW} + f_{\Delta}$$

$$\therefore \frac{f_s}{M} = a \frac{f_s}{M} + K(A) \frac{f_s}{N}$$

$$f_s \left[\frac{1-a}{M} \right] = K(A) \frac{f_s}{N}$$

$$N = M \frac{K(A)}{1-a}$$



$$\frac{N}{M} = \frac{K(A)}{1 - a}$$

N/M determined by quality specifications of filter

N = filter size, number of ops per output point

M = resample ratio, number of input points per output point

N/M = Number of Ops per input point



Example

$$K(A) = 3.6 \quad (80\text{dB})$$

$$a = 0.6$$

$$\frac{N}{M} = \frac{K(A)}{1-a} = \frac{3.6}{0.4} = 9$$

Standard filter
requires 364 Ops

Number of Ops/Input

Independent of bandwidth

Independent of sample rate

Independent of filter length

Dependent only on performance measures

fractional bandwidth (a) and out-of-band attenuation

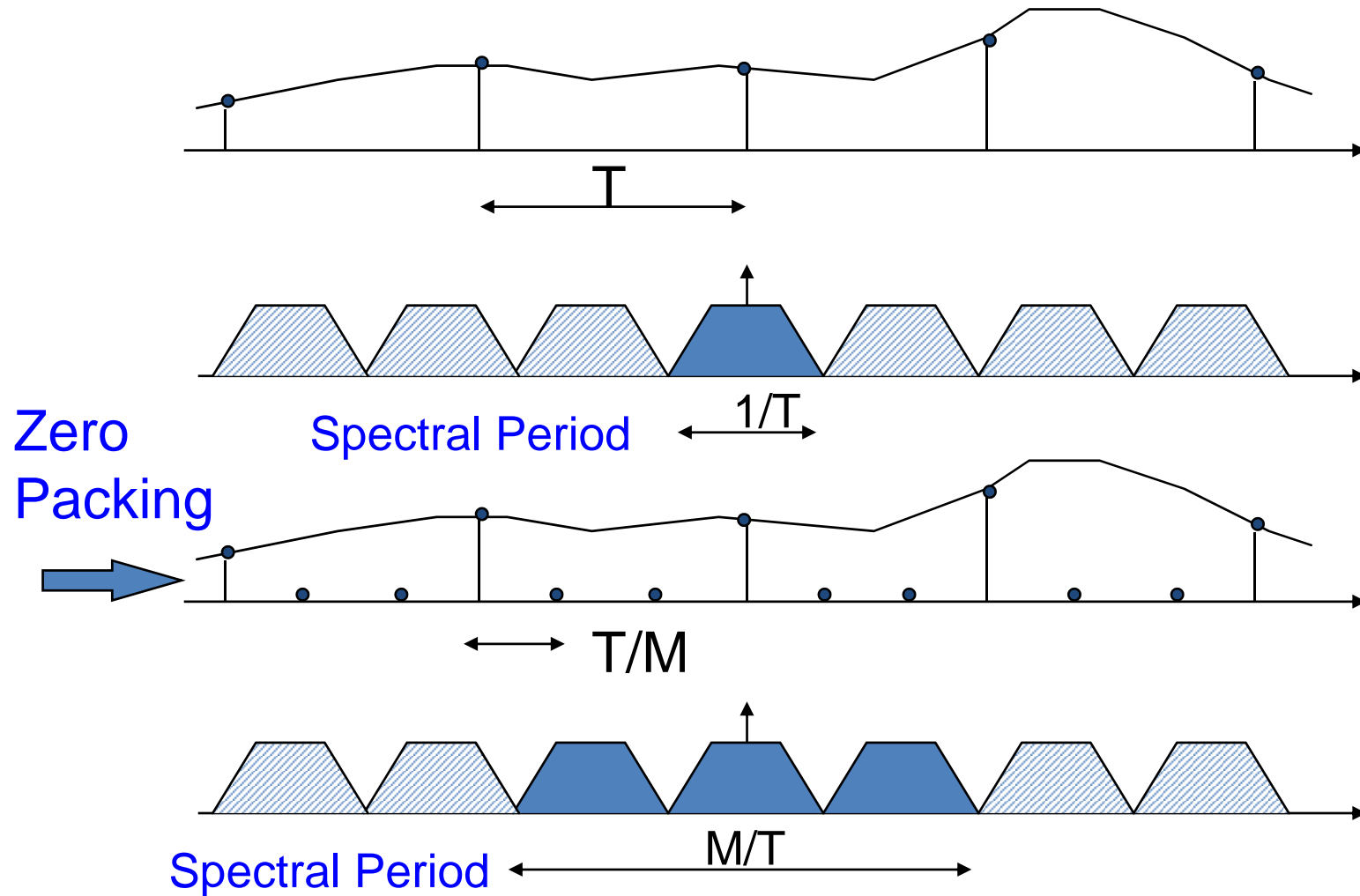


Comments

- This design formula lets the spectral replica overlap in the transition band so the attenuation never reaches the design value within the transition band.
- Need to use a filter design that has a small roll-off (say 3db per octave) in the stop band to ensure that the out of band noise does not stack up and prevent the filter from meeting specifications.

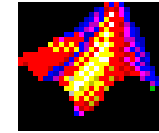


Upsampling



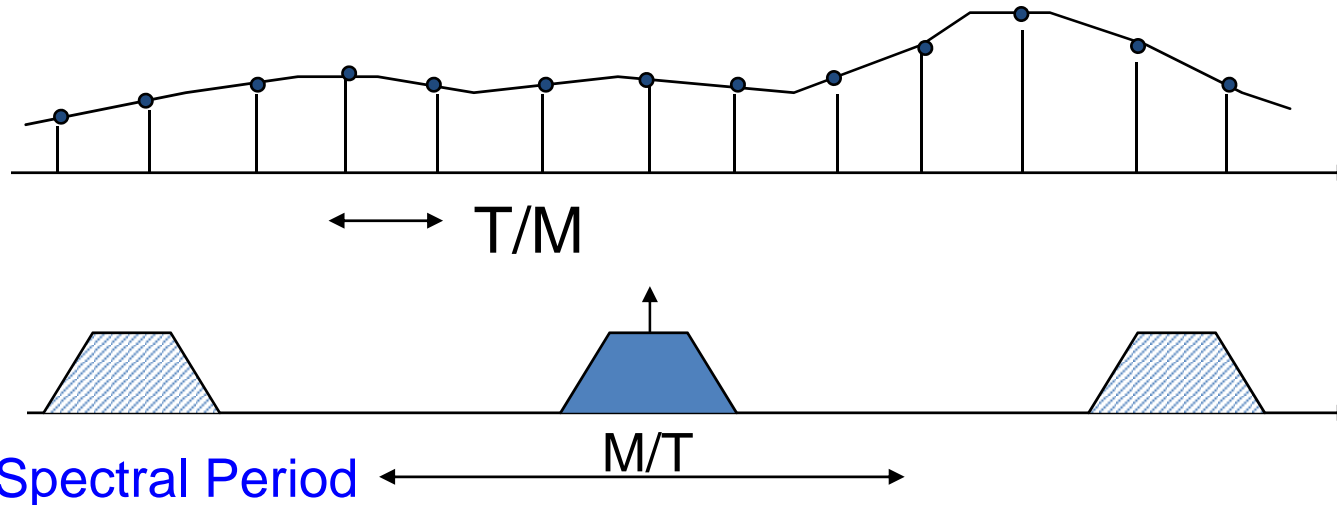


Upsampling



interp

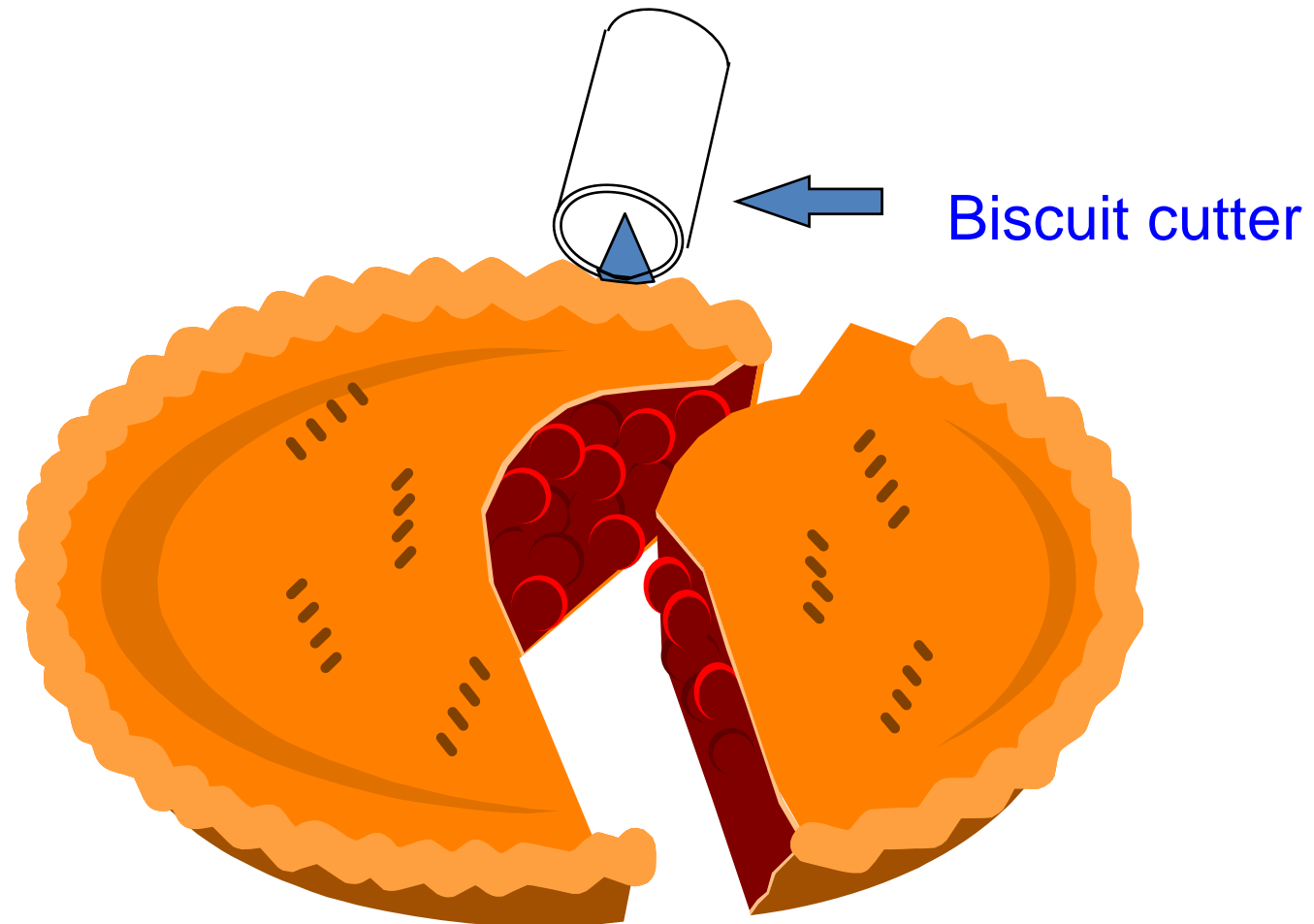
After low pass filtering to remove images
(interpolation, reconstruction, or anti-imaging filter)



Interpolation(upsampling) = zero packing and low pass filtering



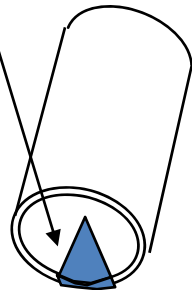
Cooking Class





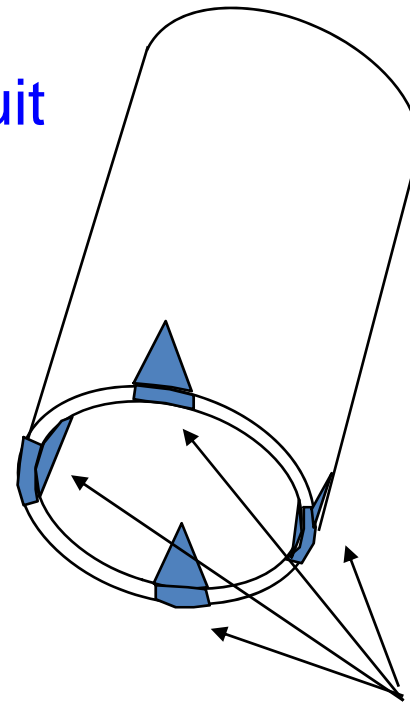
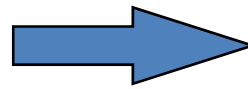
Biscuit Cutter Model of Zero-Packing and DSP Filtering

one copy



Biscuit
Cutter

New Biscuit
Cutter



four copies

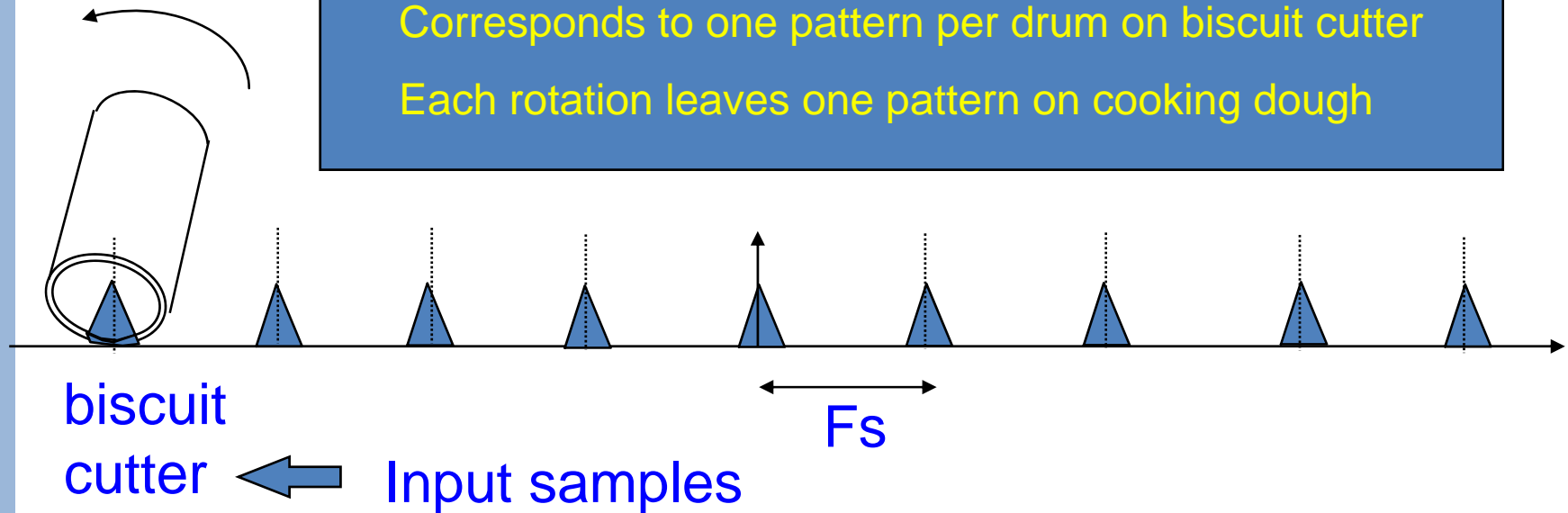


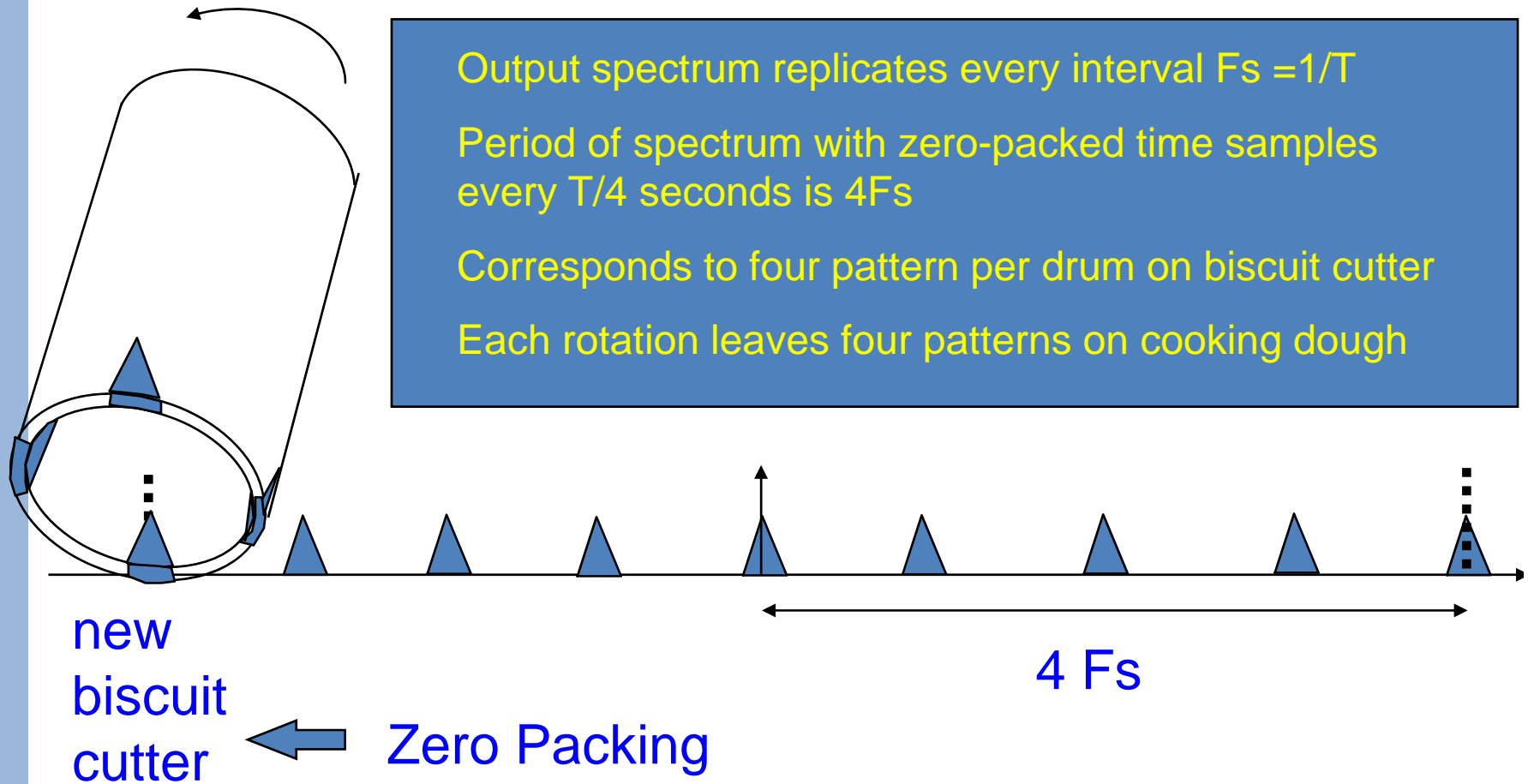
Input spectrum replicates every interval $F_s = 1/T$

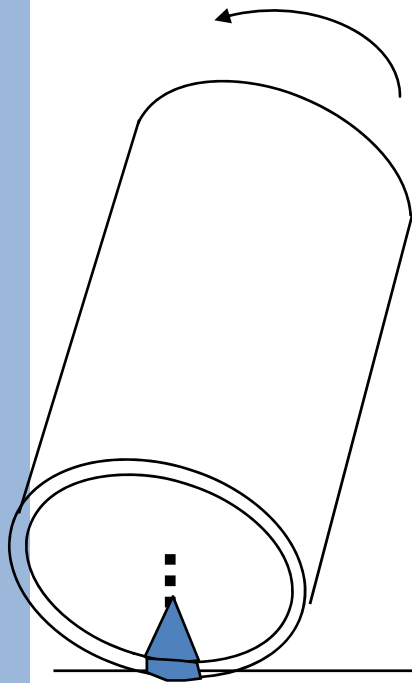
Period of spectrum with time samples every T seconds is F_s

Corresponds to one pattern per drum on biscuit cutter

Each rotation leaves one pattern on cooking dough

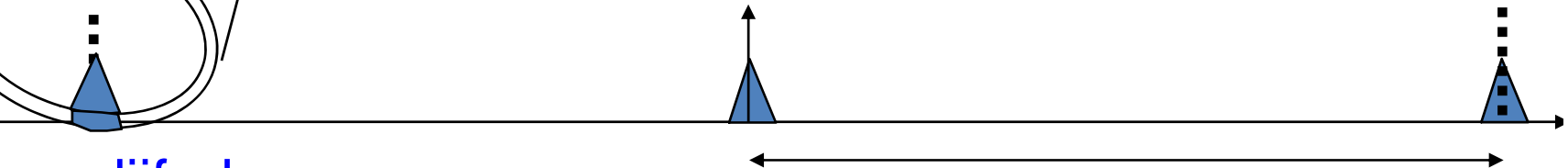




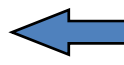


To change spectral replicating interval from F_s to $4F_s$, remove three spectral replicates from the biscuit cutter.

Then period of spectrum is $4F_s$, and zero-packed samples are replaced with bandlimited interpolated samples.



modified
biscuit
cutter

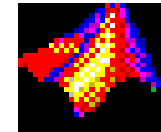


Low Pass Filter

$4 F_s$

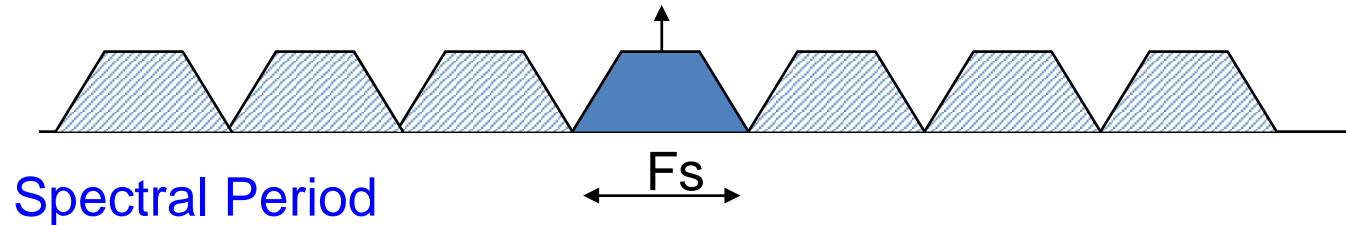


DSP Approach

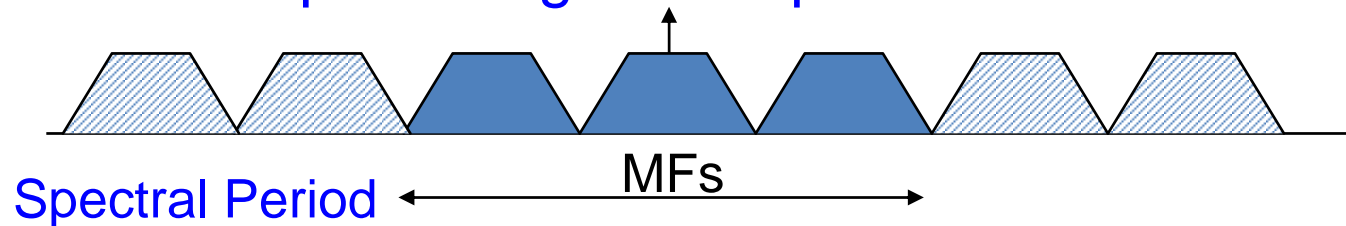


cirdemo

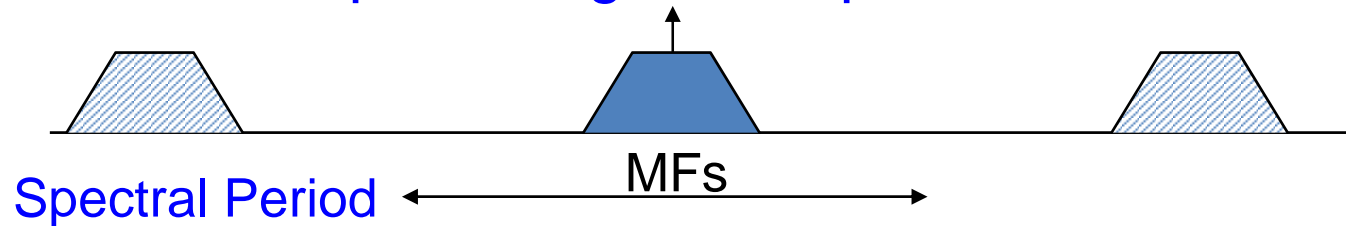
Spectrum: input to Upsampler



Spectrum: Input to Digital Lowpass



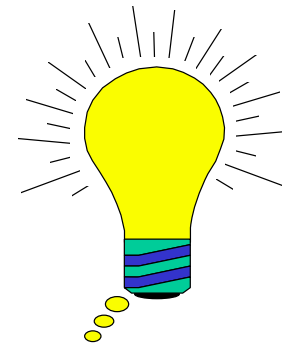
Spectrum: Output of Digital Lowpass





Comments

- We have not used the Noble Identity which says that upsampling followed by filtering can be achieved by filtering followed by upsampling.
- Thus we should implement this upsampling with a polyphase structure to reduce the computational load by a factor of M .





Polyphase Upsampler

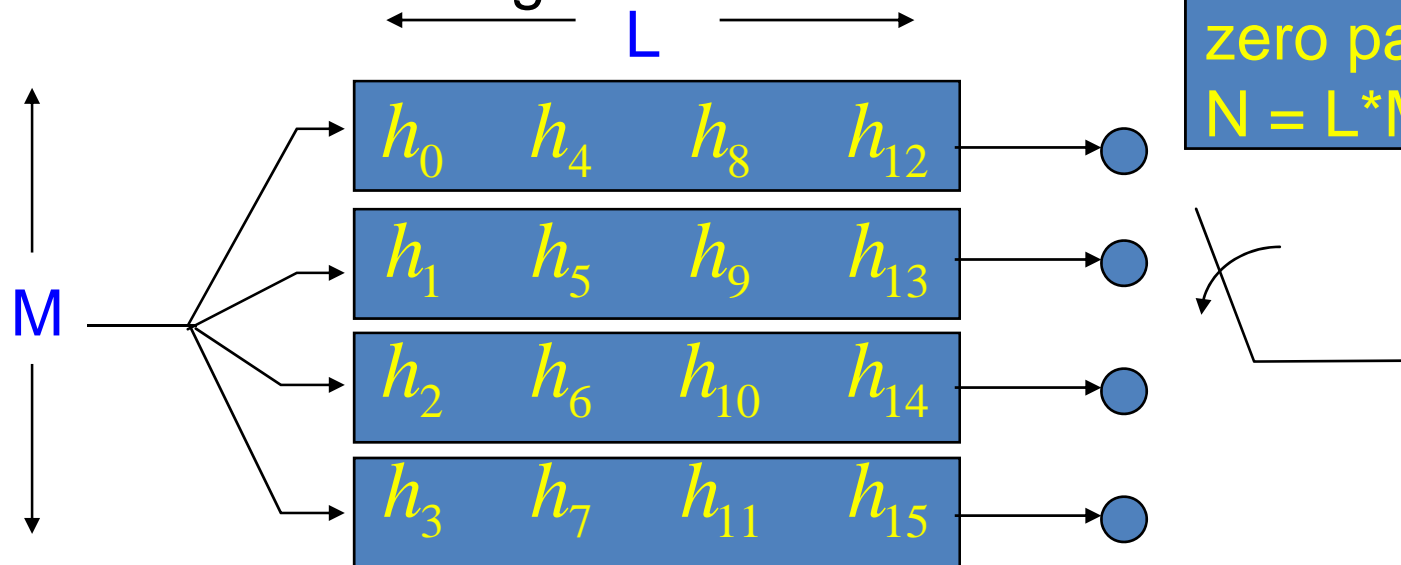
Let $N = L * M$

$N =$ Filter Length

$M =$ Resampling Rate

$L =$ Subfilter Length

Place filter coefficients columnwise into an M by L matrix. Subfilters are the rows of the matrix.



Note - can always zero pad to make $N = L * M$



Another View

